

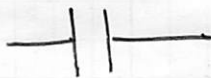

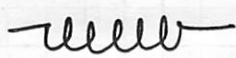
We've studied inductance generally, but now we want see how it might be used more practically. We noticed a few things about self inductance,

$$\phi = LI$$

the emf that is generated when the current changes with time $I = I(t)$, is a back emf, which reflects Lenz's Law. The EMF will be produced to fight the change,

$$\mathcal{E} = -\frac{d\phi}{dt} = -L \frac{dI}{dt}$$

In this equation we can see that the inductance, L , acts like a damping constant on the current, I . We will study the inductors in circuits so let's remind ourselves of the different circuit elements.

<u>Symbol</u>	<u>Circuit Relation</u>	<u>Geometry</u>	<u>Field</u>
	$Q = CV$ or $I = C dV/dt$	$C = \frac{\epsilon_0 A}{d}$ (Parallel plates)	$E = \sigma_b / \epsilon_0$
	$V = IR$	$R = \rho L/A$ (uniform rod)	$J = \sigma E$
	$V = -L \frac{dI}{dt}$	$L = \mu_0 n^2 A * N_{turns}^2$	$B = \mu_0 n I$ or $\Phi_B = LI$

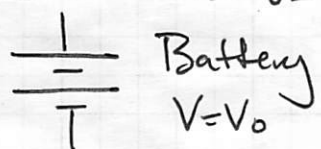
Kirchoff's Laws say, $\sum_{\text{around any closed loop}} \Delta V = 0$ and $\sum_{\text{all currents entering any node}} I_{in} = 0$

"Solving a circuit problem" means finding $I(t)$ &/or $V(t)$ for all circuit elements.

A few more notes before we get into solving problems,

Sources in circuits can be AC or DC, voltage or current sources,

Constant Voltage



Function Generators



AC Voltage Source

$$V=V_0 \sin(\omega t + \delta)$$



AC current source

$$I=I_0 \sin(\omega t + \delta)$$

More Notes:

$$\epsilon_0 = 8.85 \cdot 10^{-12} \frac{\text{farad}}{\text{m}}$$

- real capacitors range from $\underbrace{< 1 \text{ pF}}_{10^{-12} \text{ F}}$ to $\underbrace{> 1 \text{ F}}$ serious dielectrics

- Typical resistors range from $< 1 \Omega$ to several $\text{M}\Omega$
 $\sim 10^6 \Omega$

$$\mu_0 = 4\pi \cdot 10^{-7} \frac{\text{H}}{\text{m}} \quad (\text{and } L = \frac{\mu_0 N^2 A}{l}) \text{ means}$$

- real life inductors range from $< 10^{-6} \text{ H}$ to $\sim 1 \text{ Henry}$

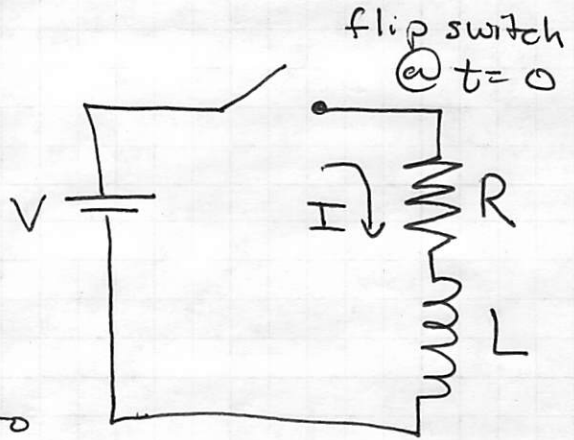
You might be worried about putting an inductor into a circuit and how we define a potential drop across it. This is where ΔV & EMF start to get a little confusing. Both are related to energy &/or work. So what we are saying when we say $\mathcal{E} = -L \frac{dI}{dt}$ is that the work per unit charge for this element is $-L \frac{dI}{dt}$ so we can use this form in Kirchoff's Law

$$\sum \Delta V = 0,$$

Example: An RL circuit.

The resistance might be distributed (in wires, battery, etc.). And so might the inductance. This is a model.

This model will allow us to see the general solution method.



Intuitively, the inductor doesn't "like" instant changes in current. We expect that at $t=0$, the current slowly changes from zero. After a long time, there are no more changes. We've reached steady state! $\Delta V_{\text{inductor}} = 0$, so it acts like an ideal wire now.

Using Kirchoff's Loop Rule we find,

$$V - IR - L \frac{dI}{dt} = 0$$

Here, we assume that $V, R, \& L$ are all known and we are seeking $I(t)$.

This equation is a 1st order, inhomogeneous ODE,

$$L \frac{dI}{dt} + IR = V$$

There are several methods to solve this ODE. We will discuss two

- ① Direct method using homogeneous & particular solutions
- ② Using the "phasors" method, which is very powerful and can be much simpler.

Method #1: Direct Solution (maybe remember from ODEs)

① Find the general homogeneous solution to:

$$L \frac{dI_H}{dt} + I_H R = 0$$

② Find some particular solution to the full (inhomog) eqn.

③ Add these solutions ($I = I_H + I_p$) to get the full solution.

④ Determine the one arbitrary constant in I_H using initial conditions.

This method works for $V = V_0$ (battery)

also if $V = V_0 \cos(\omega t)$ (AC power supply)

and thus, by superposition, we can solve for any periodic $V(t)$ because Fourier says,

$$V(t) = \sum_n V_n \cos(\omega_n t + \delta_n)$$

* This method is fairly general.

Back to the example, the homogeneous equation is,

$$\frac{dI_H}{dt} = -\frac{R}{L} I_H \Rightarrow \text{seperates simply} \Rightarrow \frac{dI_H}{I_H} = -\frac{R}{L} dt$$

$$I_H(t) = I_H(t=0) e^{-Rt/L}$$

this is an undetermined constant.

The resistor, R , kills off the current while the inductor, L , stretches that time out.

To find particular solutions, you don't need generality. Any solution that works is the solution. Guess & check is just fine.

Let's say that $V = V_0 = \text{constant}$,

$$L \frac{dI_p}{dt} + I_p R = V_0$$

Given our homogeneous solution maybe something like this works,

$$I_p(t) = a e^{-Rt/L} + b \quad \text{Let's check if this works.}$$

$$\frac{dI_p}{dt} = -\frac{R}{L} a e^{-Rt/L} \quad \text{so that,}$$

$$L \left(-\frac{R}{L} a e^{-Rt/L} \right) + (a e^{-Rt/L} + b) R = V_0$$

the exponential terms cancel! This leaves

$$bR = V_0 \quad \text{so our proposed solution works if}$$

$$b = V_0/R$$

Add the solutions together,

$$I(t) = I_p + I_H = \underbrace{(I_H(t=0) + a)}_{\text{call this a constant, } c} e^{-Rt/L} + V_0/R$$

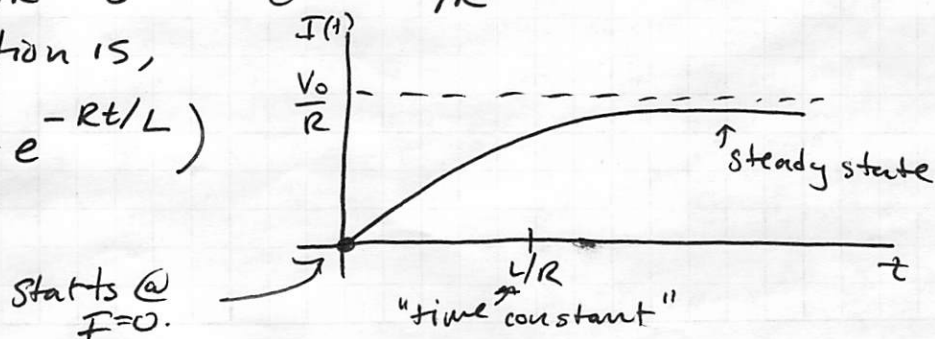
$$I(t) = C e^{-Rt/L} + V_0/R \quad \text{if at } t=0, I=0 \text{ then,}$$

$$I(0) = C + V_0/R = 0$$

So our solution is,

$$I(t) = \frac{V_0}{R} (1 - e^{-Rt/L})$$

$$C = -V_0/R$$



We will observe more interesting results when we have an AC supply. Let's work on this for,

$$V(t) = V_0 \cos(\omega t)$$

We have already found the homogeneous solution, I_H , so we just need a good guess for $I_p(t)$.

We'd expect that a sinusoidal source would result in a sinusoidal solution, so let's try,

$$I_p(t) = a \cos(\omega t + \phi)$$

← these are both undetermined coefficients.

Our differential equation is now,

$$L \frac{dI_p}{dt} + I_p R = V_0 \cos(\omega t)$$

$$-L\omega a \sin(\omega t + \phi) + aR \cos(\omega t + \phi) = V_0 \cos(\omega t)$$

this looks a little complex but we can simplify things ~~with~~ with standard trig identities,

$$\sin(a+b) = \sin a \cos b + \cos a \sin b$$

$$\cos(a+b) = \cos a \cos b - \sin a \sin b$$

If we use these identities we find,

$$-L\omega a \sin \omega t \cos \phi - aR \sin \omega t \sin \phi = 0$$

$$-L\omega a \cos \omega t \sin \phi + aR \cos \omega t \cos \phi = V_0 \cos \omega t$$

if the coeffs in front of the $\sin \omega t$ terms vanish and those in front of the $\cos \omega t$ terms give V_0 , it works!

$$\left. \begin{aligned} -L\omega a \cos \phi - aR \sin \phi &= 0 \\ -L\omega a \sin \phi + aR \cos \phi &= V_0 \end{aligned} \right\} \begin{array}{l} \text{Two eqns and} \\ \text{two unknowns } (a \text{ and } \phi) \end{array}$$

⇒ the first equation we have gives

$$-L\omega \cos\phi = aR \sin\phi$$

• if $a=0$, this works, but that means $I_p(t) = 0$

• if instead, $\tan\phi = -\frac{L\omega}{R}$ or $\boxed{\phi = \tan^{-1}\left(-\frac{L\omega}{R}\right)}$

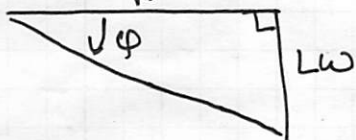
then we get a nonzero I_p .

So ϕ is not an arbitrary constant and is not dependent on initial conditions. It is determined by the circuit elements and the driver.

⇒ the second equation we have gives,

$$a(-L\omega \sin\phi + R \cos\phi) = V_0$$

We can use a triangle that shows $\tan\phi = -\frac{L\omega}{R}$,



We can read off $\sin\phi$ & $\cos\phi$,

$$\sin\phi = \frac{-L\omega}{\sqrt{R^2 + L^2\omega^2}} \quad \cos\phi = \frac{+R}{\sqrt{R^2 + L^2\omega^2}}$$

Let's put these back into the 2nd equation,

$$a \left(\frac{L^2\omega^2}{\sqrt{R^2 + L^2\omega^2}} + \frac{R^2}{\sqrt{R^2 + L^2\omega^2}} \right) = a \left(\sqrt{R^2 + L^2\omega^2} \right) = V_0$$

$$\boxed{a = \frac{V_0}{\sqrt{R^2 + L^2\omega^2}}}$$

So with $\phi = \tan^{-1}\left(-\frac{L\omega}{R}\right)$ and $a = \frac{V_0}{\sqrt{R^2 + L^2\omega^2}}$,

$I_p(t) = a \cos(\omega t + \phi)$ works.

So our full solution is,

$$I(t) = I_p + I_H = a \cos(\omega t + \varphi) + I_{H0} e^{-Rt/L}$$

= persistent oscillatory response + dying away piece

\Rightarrow a and φ are determined already (on previous page)

I_{H0} is not determined; it is determined by initial conditions.

So if, for example, at $t=0$, $I=0$ then,

$$I(t > 0) = a \cos(\omega t + \varphi) - \underbrace{a \cos \varphi}_{\text{makes } I(t=0)=0} e^{-Rt/L}$$

with amplitude $a = \frac{V_0}{\sqrt{R^2 + L^2 \omega^2}}$ and phase, $\varphi = \tan^{-1}\left(\frac{-L\omega}{R}\right)$

- When R is large, a is small. Big R kills off long term currents.
- When $\omega = 0$ (battery), $a \rightarrow V_0/R$ and $\tan^{-1}(0) = 0 = \varphi$.
the inductor acts like an ideal wire in the long term limit w/ DC voltage.
- When $\omega \rightarrow \infty$, $a \rightarrow 0$; Inductors don't like rapid changes (big Back EMFs!)
they will suppress response at high f .

This method works just fine, but it's a real pain when you have a more complex circuit. especially w/ multiple R 's, L 's, & C 's in series and/or parallel.

Method 2 Phasors

- The phasor method is a bit more sophisticated, but it's incredibly powerful and widely used.
- It gets rid of the sines & cosines and changes our problem to a simple algebra problem using exponentials.
- We will make use of Euler's famous formula,

$$e^{i\theta} = \cos\theta + i\sin\theta$$
 or for our purposes,

$$e^{i\omega t} = \cos\omega t + i\sin\omega t.$$

What's nice about the exponential form is how they work under derivatives (and integrals),

$$\frac{d}{dt}(\cos\omega t) = -\omega\sin\omega t \text{ is a new, linearly ind. function (leads to complications.)}$$

But,

$$\frac{d}{dt}(e^{i\omega t}) = i\omega e^{i\omega t}, \text{ just proportional to the original function, } \frac{df}{dt} \propto f. \text{ (much easier!)}$$

So here's what we are going to do. Instead of $V_0\cos\omega t$ as the driver, we will use $V_0 e^{i\omega t}$. Now, this might bother you b/c the voltage is complex. That's fine, at the end of the day we will take the Real Part.

$$V_{true} = \text{Re}[V_{fictional}] \text{ and } I_{true} = \text{Re}[I_{fictional}]$$

We can do this b/c the ODE is linear, so $\text{Re}(I)$ arises from $\text{Re}(V)$. The ODE will be simpler, but we will have to remember to take the real part.

Lets rework the problem again using the phasor method,

$$L \frac{dI}{dt} + IR = V(t) = \tilde{V} e^{i\omega t}$$

so we have this (fictious) driving voltage, $\tilde{V} e^{i\omega t}$. It's complex

- the real voltage is $\text{Re}(\tilde{V} e^{i\omega t})$
- if \tilde{V} is itself a complex constant (i.e., $\tilde{V} = V_0 e^{i\delta}$), then we can have more complex drivers $V_0 \cos(\omega t + \delta)$

We know the solution for I_H , so we just need to find I_p .

We will guess & check. This time we guess a

simple form: $I_p = \tilde{I} e^{i\omega t}$

$$L \frac{dI_p}{dt} + I_p R = \tilde{V} e^{i\omega t} \quad \text{is the ODE,}$$

$$L \tilde{I} (i\omega) e^{i\omega t} + \tilde{I} R e^{i\omega t} = \tilde{V} e^{i\omega t} \quad \text{the } e^{i\omega t} \text{'s cancel out!}$$

$$L \tilde{I} (i\omega) + \tilde{I} R = \tilde{V} \quad \text{or} \quad \tilde{I} = \frac{\tilde{V}}{R + i\omega L}$$

that's it! \tilde{I} is a constant \rightarrow and our solution

is simply,

$$I_{\text{true}} = \text{Re}(I_{\text{fictious}}) = \text{Re}(\tilde{I} e^{i\omega t}) + I_H$$

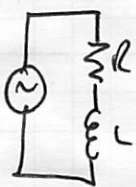
see how much simpler that is!

from before

The solution looks like $\tilde{V} = \tilde{I} \tilde{R}$ with \tilde{R} now complex

\tilde{R} is the impedance (or complex impedance), we label it Z

for



We got $Z = R + i\omega L$

a series circuit just add the impedances

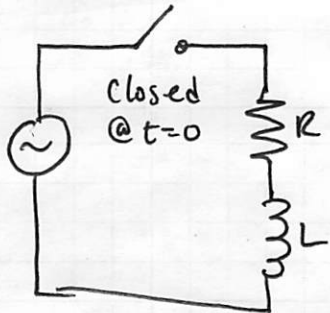
more general (actually!)

$$Z_R = R \quad \text{resistor}$$

$$Z_L = i\omega L \quad \text{inductor}$$

(turns out a capacitor has $Z_C = \frac{-i}{\omega C}$)

Let's return to the RL example and wrap it up,



$$Z_{++} = R + i\omega L$$

so we have, $\tilde{V} = \tilde{I}(R + i\omega L)$

and $V_{me} = \text{Re } \tilde{V} e^{i\omega t}$

$$I_{me} = \text{Re } \tilde{I} e^{i\omega t} = \text{Re} \left(\frac{\tilde{V} e^{i\omega t}}{R + i\omega L} \right)$$

In our original setup, $V_{real} = V_0 \cos \omega t$ so $\tilde{V} = V_0$

So we have:

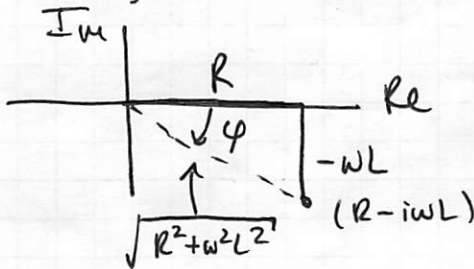
$$I_{me} = \text{Re} \left(\frac{V_0 e^{i\omega t}}{R + i\omega L} \right) = \text{Re} \left(\frac{V_0 e^{i\omega t}}{R + i\omega L} \frac{R - i\omega L}{R - i\omega L} \right)$$

Standard method \uparrow

$$\text{So, } I = \frac{V_0}{R^2 + \omega^2 L^2} \text{Re} (e^{i\omega t} (R - i\omega L))$$

How do we deal with the rest of the expression?

Another standard method, draw $R - i\omega L$ in the complex plane,



In the complex plane,

this point is simply,

$$\sqrt{R^2 + \omega^2 L^2} e^{i\phi} \quad \text{with } \phi = \tan^{-1} \left(\frac{-\omega L}{R} \right) \quad \text{as before}$$

$$\text{So, } I = \frac{V_0}{\sqrt{R^2 + \omega^2 L^2}} \text{Re} (e^{i\omega t} e^{i\phi}) = \frac{V_0}{\sqrt{R^2 + \omega^2 L^2}} \cos(\omega t + \phi)$$

this is the exact solution we had before but now $V = IZ$

This works for $V = V_0 \cos(\omega t + \delta) \Rightarrow$ use $\tilde{V} = V_0 e^{i\delta}$

or for $V = V_0 \sin(\omega t) \Rightarrow$ use $\tilde{V} = V_0 e^{i\pi/2}$

What if there's a capacitor? Can we use the same tools?

$$-||- \quad V = \frac{Q}{C} \Rightarrow \frac{dV}{dt} = \frac{I}{C} \quad \text{or that } I = C \frac{dV}{dt}$$


So if the driver is $V(t) = \tilde{V} e^{i\omega t}$ then,

$$I = C i\omega \tilde{V} e^{i\omega t} = i\omega C V$$

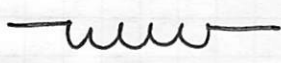
This looks like $V = I "R"$ but this time the

impedance is $Z_C = \frac{1}{i\omega C} = \frac{-i}{\omega C}$ (we use Z to indicate complex impedance)

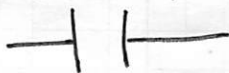
Summary

$$Z = R$$


R

$$Z = i\omega L$$


L

$$Z = -i/\omega C$$


C

General Result! you can treat each passive element like a simple resistor with the impedances given above. You can construct Z_{eff} using the standard "rules" for resistors.

In series,

$$Z_{\text{eff}} = Z_1 + Z_2 + Z_3 + \dots$$

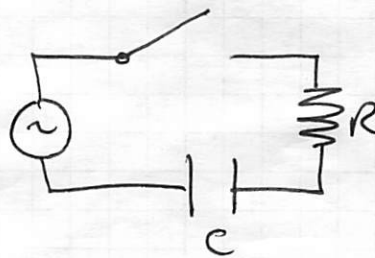
In parallel,

$$\frac{1}{Z_{\text{eff}}} = \frac{1}{Z_1} + \frac{1}{Z_2} + \frac{1}{Z_3} + \dots$$

Can apply usual Kirchhoff's Laws to them as well.

Example! An RC circuit

Turn it on @ $t=0$
with $V(t) = V_0 \cos \omega t$



think of this as two Z 's,

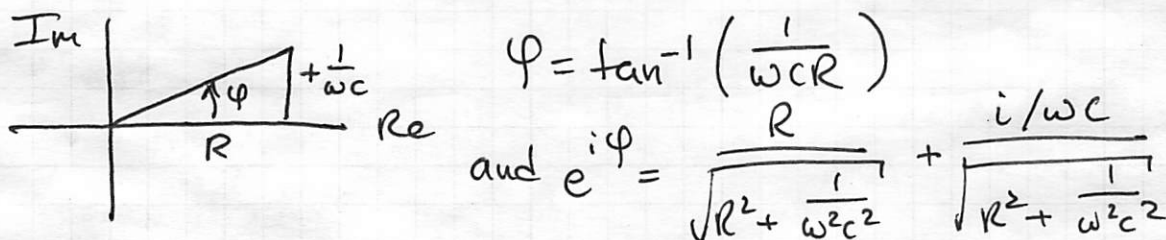
$$Z_{\text{tot}} = Z_R + Z_C = R - i/\omega C$$

with, $\tilde{V} = \tilde{I} Z \Rightarrow \tilde{I} = \frac{\tilde{V}}{R - i/\omega C}$ and $I_{\text{real}} = V_0 \operatorname{Re} \left(\frac{e^{i\omega t}}{R - i/\omega C} \right)$

the first part uses this method again,

$$\tilde{I} = V_0 \operatorname{Re} \left(\frac{e^{i\omega t}}{R - i/\omega C} \frac{R + i/\omega C}{R + i/\omega C} \right) = \frac{V_0}{R^2 + \frac{1}{\omega^2 C^2}} \operatorname{Re} \left(e^{i\omega t} \left(R + \frac{i}{\omega C} \right) \right)$$

Use the second method, draw a picture,



So the particular solution is,

$$I_p = \frac{V_0}{\sqrt{R^2 + \frac{1}{\omega^2 C^2}}} \cos(\omega t + \varphi)$$

We still need to solve the homogeneous equation,

$$0 = IR + Q/C \Rightarrow \frac{dI}{dt} R = -\frac{I}{C}$$

take time derivative
($dQ/dt = I$)

So, $\frac{dI}{I} = -\frac{1}{RC} dt \Rightarrow I_H = I_0 e^{-t/RC}$

So $I_{\text{tot}} = \underbrace{\frac{V_0}{\sqrt{R^2 + \frac{1}{\omega^2 C^2}} \cos(\omega t + \varphi)}_{\text{Steady solution}} + \underbrace{I_0 e^{-t/RC}}_{\substack{\uparrow \text{transient} \\ \text{dies off} \\ \text{by initial} \\ \text{conditions.}}}$

Initial Conditions: ΔV_{cap} cannot suddenly change.

If it was zero before then just after $V_0 = IR$ b/c $\Delta V_{cap} = 0$ for just a quick moment. So $I(t=0) = V_0/R$.

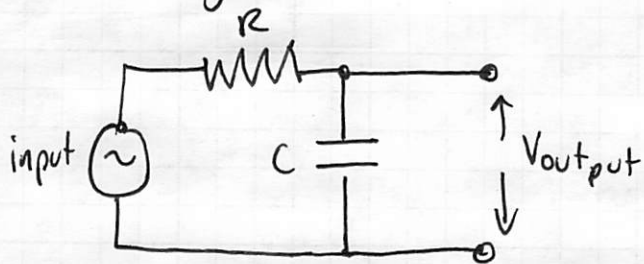
So, this gives,

$$I(t) = \frac{V_0}{\sqrt{R^2 + 1/\omega^2 C^2}} \cos(\omega t + \phi) + \left(\frac{V_0}{R} - \frac{V_0 \cos \phi}{\sqrt{R^2 + 1/\omega^2 C^2}} \right) e^{-t/RC}$$

Picked so @ $t=0$ $I = V_0/R$.

- time constant is "RC"
- After waiting several RC times the circuit oscillates with driver frequency, ω
- If $\omega \rightarrow 0$, $I_{long term} \rightarrow 0$, the capacitor blocks steady current.
- if $\omega \rightarrow \infty$, $I_{long term} \rightarrow \frac{V_0}{R} \cos(\omega t)$ like the capacitor isn't there.

It's often useful to put this setup in a circuit where you can read out a voltage (as a signal)



We know I in this circuit and V_{out} is,
 $V_{out} = I Z_C = I (-i/\omega C)$

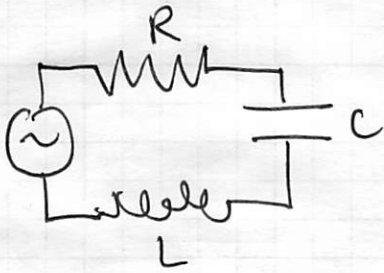
$$V_{out} = \frac{V_{in}}{Z_{tot}} Z_C = \frac{V_{in}}{R - \frac{i}{\omega C}} (-i/\omega C) = V_{in} \left(\frac{1}{1 + i\omega RC} \right)$$

With $\omega \rightarrow 0$, $V_{out} = V_{in}$, cap does nothing

with $\omega \rightarrow \infty$, $V_{out} \rightarrow 0$, "low pass filter"

Allows low frequencies to pass; suppresses high frequency.

With the phasor method & impedance, any circuit is basically a 184 circuit.



just use $Z = R + i\omega L - \frac{i}{\omega C}$

and then $\tilde{V} = \tilde{I} \tilde{Z}$